

HOT PRESSING CERAMIC DISTORTION CONTROL

BACKGROUND OF THE INVENTION

5 The present invention is directed to the control of distortion during high temperature processing, and, more particularly, in the hot pressing of metallized multilayer ceramic (MLC) substrates.

10 In the manufacture of MLC substrates, ceramic greensheets are formed from a casting slurry. The individual ceramic greensheets are personalized with via holes and conductive metal. The ceramic greensheets are then stacked together in a predetermined design sequence to form a green ceramic laminate. After the greensheets are stacked, heat and pressure are applied to the greensheets to provide a green ceramic laminate with continuous conductive metal wiring whose layers will remain contiguous during subsequent processing.

15 This process of applying heat and pressure to the stacked greensheets is called lamination. The green ceramic laminate is then fired in a process called sintering, where the green laminate is densified under heat and pressure. The process of sintering ceramic under uniaxially applied pressure is also known as hot pressing. When the pressure is applied in all directions, then the sintering process is typically known as hot isostatic

5 pressing. In contrast, free sintering typically refers to the process of sintering under no external load or pressure.

 During the hot pressing process, employed primarily for densifying the ceramic and the conductive metal materials in MLC substrates, large volume shrinkage of the MLC substrate typically occurs. More specifically, in the case of hot pressing, when the pressure is applied in one direction, the volume shrinkage experiences significant non-uniform viscous deformation throughout the densifying body. Since both the densification and viscous deformation processes are typically dependent on the sample viscosity, these two processes happen simultaneously but at different deformation rates which are temperature sensitive. In addition, when hot pressing MLC products, the densification process will also be dependent on the distribution of metal phase while being somewhat insensitive to external conditions, mainly because the primary driving force for densification is the ceramic phase surface tension. In contrast, the viscous deformation process will have a strong dependency on all external forces applied to the sample.

20 In general the ceramic and conductive metal materials have a wide difference in physical and transport properties. The onset of densification and the densification profiles between the ceramic and metal phases differ widely as well. With application of external pressure during the sintering process, some of the differences in densification rates may be reduced when the metal densification rate is sensitive to applied pressure. But the use

5 of uniaxial external pressure during densification creates viscous deformation in the sample as well. The complex densification process of the composite, in conjunction with the viscous deformation rate result in distortion, both in the pattern of the conductive metal features and in the substrate body dimensions.

10 Distortion is defined as deviation in actual post sinter dimensions from the ideal design dimensions. Distortion in the body dimensions includes deviation in surface flatness called camber. Distortion control in sintering by hot pressing processes requires the conductive metal and the ceramic material to have similar shrinkage rates, the application of external pressure at a rate consistent with the ceramic-metal composite physical properties, and careful selection of the method to apply the pressure to the product. However, even with careful selection of materials, variations in material from lot to lot can result in unpredictable shrinkage due to, for example, contamination or particle size distribution. Further, the application of external pressure to the densifying sample may also introduce processing related variations, such as load variation, which can result in product to product variation on a given sample batch and generate product distortion.

15 In MLC substrates this distortion can manifest itself as substrate warping, substrate camber, and variations in substrate dimensions. High distortion results in product with low yield and increased production costs.

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Hot pressing is typically used to densify ceramic-metal composites at lower

5 temperatures than what is needed to complete the same process using a free sintering
method. The use of external pressure during densification also helps the control of
substrate camber during densification when the difference in shrinkage rate between the
ceramic phase and the metal phase is significant and can not be reduced adequately by
conventional means such as particle size distribution and material chemistry. In some
10 applications, the use of external pressure is the only manufacturable process feasible to
generate a given ceramic-metal composite. But the use of external pressure during
sintering introduces many complexities into the sintering process which impact directly
on the manufacturing costs.

15 For example, the use of external pressure during sintering requires the use of
specially designed hardware to transfer the pressure to the product under densification.
Sintering hardware should not restrict the product heating, cooling, or any chemical
reaction involving mass transport, and should not deform significantly under pressure.
Also, the hardware used to apply the sintering pressure uses up valuable furnace volume.
Thus, higher external sintering pressure and temperature translates directly into more
20 expensive hardware to carry out the already costly sintering process.

Not surprisingly then, the hot pressing process is significantly more expensive
than free sintering for a given manufacturing production rate. To reduce cost, each sample
being hot pressed may include many final products, which are typically separated in a

5 subsequent post-sinter dicing operation. Unfortunately, the effort to control laminate distortion during hot pressing increases the difficulty significantly when the laminate includes multiple products. This is mainly because in a typical multi-up laminate the space between the individual product samples, or "ups", is free of metallurgy. The viscoelastic properties of the sintering laminates are dependent on metallurgy distribution and therefore multiup laminate sintering inherently has built in variations in physical and transport properties.

The manufacture of MLC substrates involves multiple processes which directly impact the product dimensions and distortion during the sintering step. Extensive effort is expended at increased cost to control the post sinter MLC substrate dimensions.

15 Advances in microelectronic technology has continuously increased the number of chip input/output "I/O", while decreasing the corresponding chip size. This creates a demand for MLC substrates with reduced top surface metal (TSM) interconnect dimensions. Correspondingly the MLC substrate bottom surface I/O pad density needs to be increased. Such a design need increases the challenge of product build, in particular product dimensional control. Therefore, there is a need for cost-effective distortion control in MLC substrate manufacturing.

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There are a number of methods employed currently to control substrate dimensions during MLC substrate manufacturing that are applicable to ceramic-metal

5 systems which are densified under free sintering conditions. However, methods which
can be used when the densification is done under external pressure are limited.
Sometimes, an additional sinter process under pressure is applicable and will reduce
ceramic distortion in some material systems. However this process is expensive and
results in additional product yield loss. Often this process is not possible. Additionally,
10 tailoring the type of conductive metal used throughout the substrate may be employed to
control product distortion, but this is not useful to control global distortion.

Also, this solution is not comprehensive and does not always address the problem
of individual product distortion. Selective distribution of the conductive metal throughout
the individual product, to the maximum extent possible, can bound individual product
15 distortion but fails to control global distortion problems. Greensheet stack lamination
pressure adjustment is sometimes used to control global distortion. However this
technique is not as effective when used with hot pressing. Finally, product redesign may
be used as a tool to reduce distortion in some cases by adjusting the conductive metal
distribution in key areas. However, this is undesirable since it is very costly and impacts
20 new product time to market. The existing procedures and models used to control product
dimensions are not fully predictive, and are therefore not dependable and quite limiting.

There are methods proposed by others to improve the dimensional control of
electronic packages. Natarajan et al. U.S. Pat. No. 6,627,020, the disclosure of which is

5 incorporated by reference herein, discloses the use of discrete non-densifying structures to control the dimensions of a free sintered multilayer ceramic substrate. Robbins et al. U.S. Pat. No. 5,801,073, the disclosure of which is incorporated by reference herein, discloses a method for producing an electronic packaging device made of dissimilar materials within a package. Robbins discloses a method to achieve minimal overall shrinkage of the
10 package by the use of a high purity reaction bonded silicon nitride as a dielectric ceramic material.

Mori et al. U.S. Pat. No. 5,370,760, the disclosure of which is incorporated by reference herein, discloses a method to reduce the distortion of the metallized features in a ceramic laminate during the lamination process prior to sintering. Mori discloses the use
15 of a die assembly, which is a tool, having an outer portion and an inner portion which can compress the outer peripheral portion of the laminate to a higher degree than the central portion of the laminate. This disclosure does not address the control of distortion induced during the sintering process.

Notwithstanding the prior art there remains a need to minimize the external
20 sintering pressure and control the dimensions of MLC substrates already designed, but which fail to meet their post sinter dimensional requirements, and whose overall distortion is not amenable to the existing dimensional control methods.

5 These and other purposes of the present invention will become more apparent after referring to the following description considered in conjunction with the accompanying drawings.

BRIEF SUMMARY OF THE INVENTION

10 The purposes of the present invention have been achieved by providing, according to a first embodiment, a method to control the post sinter dimensions of a multilayer ceramic substrate sintered under load comprising the steps of:

 providing at least one first continuous non-densifying structure;

 providing at least one personalized ceramic greensheet having a local peripheral kerf area and an external peripheral kerf area;

15 placing the first continuous non-densifying structure on the local peripheral kerf area of the personalized ceramic greensheet;

 placing the personalized ceramic greensheet having the first continuous non-densifying structure in a stack of personalized greensheets;

20 laminating the stack of personalized ceramic greensheets to form a green ceramic laminate wherein the first continuous non-densifying structure will at least partially control the dimensions of the green ceramic laminate during lamination;

 sintering the green ceramic laminate under load to form a multilayer ceramic

5 substrate wherein the first continuous non-densifying structure will at least partially control the dimensions of the multilayer ceramic substrate during sintering.

 The method may further comprise the steps of post sinter sizing the multilayer ceramic substrate thereby separating the first continuous non-densifying structure from the multilayer ceramic substrate.

10 The method may further comprise the steps of:
 providing a second continuous non-densifying structure;
 placing the second continuous non-densifying structure on the external peripheral
kerf area of the personalized ceramic greensheet prior to lamination wherein the
second continuous non-densifying structure will at least partially control the
15 dimensions of the green ceramic laminate during lamination, and
 pre-sinter sizing the green ceramic laminate thereby separating the second
continuous non-densifying structure from the green ceramic laminate prior to
sintering.

 In another embodiment of the present invention there is provided a method to
20 control the post sinter dimensions of a multilayer ceramic substrate which is
laminated and sintered under load as a multi-up green ceramic laminate comprising
the steps of:

5 providing at least one first continuous non-densifying structure;
 providing at least one personalized ceramic greensheet having a plurality of
product samples separated by a local kerf area and having peripheral external kerf
area;
 placing the first continuous non-densifying structure on the local kerf area of the
10 personalized ceramic greensheet;
 placing the personalized ceramic greensheet having the first continuous non-
densifying structure in a stack of personalized greensheets;
 laminating the stack of personalized ceramic greensheets to form a multi-up green
ceramic laminate wherein the first continuous non-densifying structure will at least
15 partially control the dimensions of the multi-up green ceramic laminate during
lamination;
 sintering the green ceramic laminate under load to form a multi-up multilayer
ceramic substrate wherein the first continuous non-densifying structure will at least
partially control the dimensions of the multi-up multilayer ceramic substrate during
20 sintering.

The method may further comprise the steps of post sinter sizing the multi-up
multilayer ceramic substrate to form individual multilayer ceramic substrates and
thereby separating the first continuous non-densifying structure from the individual
multilayer ceramic substrates.

5 The method may further comprise the steps of:
 providing at least one second continuous non-densifying structure;
 placing the second continuous non-densifying structure on the external peripheral
kerf area of the personalized ceramic greensheet prior to lamination wherein the
second continuous non-densifying structure will at least partially control the
10 dimensions of the multi-up green ceramic laminate during lamination, and
 pre-sinter sizing the multi-up green ceramic laminate thereby separating the
second continuous non-densifying structure from the multi-up green ceramic laminate
prior to sintering.

 In another embodiment of the present invention there is provided a multilayer
15 ceramic laminate structure comprising:
 a plurality of laminated ceramic greensheets;
 at least one personalized ceramic greensheet having a local peripheral kerf area
and an external peripheral kerf area;
 at least one first continuous non-densifying structure placed on the local
20 peripheral kerf area of the personalized ceramic greensheet.

 The multilayer ceramic laminate structure may further comprise at least one
second continuous non-densifying structure placed on the external peripheral kerf

5 area.

In another embodiment of the present invention there is provided a multi-up multilayer ceramic laminate structure comprising:

a plurality of laminated ceramic greensheets;

10 at least one personalized ceramic greensheet having a plurality of product samples separated by a local kerf area and having peripheral external kerf area;

at least one first continuous non-densifying structure placed on the local kerf area of the personalized ceramic greensheet.

15 The multi-up multilayer ceramic laminate structure may further comprise at least one second continuous non-densifying structure placed on the external peripheral kerf area.

BRIEF DESCRIPTION OF THE DRAWINGS

The features of the invention believed to be novel and the elements characteristic of the invention are set forth with particularity in the appended claims. The Figures are for illustration purposes only and are not drawn to scale. The invention itself, however,

5 both as to organization and method of operation, may best be understood by reference to the detailed description which follows taken in conjunction with the accompanying drawings in which:

Figure 1A is a schematic top view of a conventional metallized ceramic greensheet.

10 Figure 1B is a schematic side view of a conventional green ceramic laminate.

Figure 2A is a schematic top view of a metallized ceramic greensheet with inventive continuous non-densifying structures added to control distortion.

Figure 2B is a schematic side view of a green ceramic laminate with inventive continuous non-densifying structures added to control distortion.

15 Figures 3 - 5 present schematic views of the use of the inventive continuous non-densifying structures on multiple layers and locations in a green laminate to control distortion.

5 **DETAILED DESCRIPTION OF THE INVENTION**

 During MLC sintering, the green ceramic laminate undergoes a large volume change, typically from about 40% to about 60% shrinkage, to produce the final MLC substrate. In the case of a free sintering process, the MLC substrate shrinks in all three dimensions, typically about 10% to about 20% linearly in each dimension. If the sintering is done under load, then one dimension may experience most of the shrinkage, particularly in the direction of the applied load. This is directly dependent on the method used to apply the sintering pressure to the green ceramic laminate. In both free sintering and sintering under load, the MLC substrate shrinkage occurs during the ceramic densification stage. During this stage the viscosity of the MLC substrate is sufficiently low and allows the internal sintering forces, driven predominantly by surface tension, to shrink the MLC substrate to its final dimensions. The present invention is directed to control distortion during sintering under load.

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 Interaction between the ceramic and metal phases in the green ceramic laminate determines some of the final MLC substrate dimensions, and consequently defines yield levels. Because of their different physicochemical nature, the metal and ceramic phases densify at a different onset and rate. This difference in densification rate directly contributes to the deviation of the post sinter MLC substrate dimensions from design dimensions, primarily because the metal phase in a typical MLC laminate is not

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5 uniformly distributed.

In addition, the use of different types of metallurgy in a given ceramic laminate also contributes to substrate distortion during sintering. Both said distortion inducing factors are unavoidable in MLC manufacturing because they are necessary for the electrical and mechanical interconnection function, which the substrate provides between
10 the integrated circuit chip and electronic card.

The present invention is applicable to any personalized ceramic greensheet. A personalized ceramic greensheet may or may not be metallized. The term "personalized" refers to a ceramic greensheet which has been selected for use in the laminate because of a particular characteristic. While this characteristic is typically the metallized pattern
15 screened on the sheet it could also refer to a particular characteristic of a blank or non-metallized sheet such as its thickness. Where the personalized ceramic greensheet is metallized the conductive metal may be, for example, molybdenum, nickel, copper, tungsten, metal-ceramic conductors and metal-glass conductors. The personalized ceramic greensheet may consist of, for example, alumina, borosilicate glass-ceramic or
20 aluminum nitride.

Referring to Figure 1A there is shown a top view of a typical metallized green sheet 10. In this particular example the green sheet 10 contains four ceramic products 35,

5 or four ups, an external kerf area **20** which will be green sized away before sintering, and
a local kerf area **30** surrounding and separating the ceramic products **35** which will be
separated away from the ceramic products or ups **35** after sintering. This is usually
accomplished with a wet sizing process. Figure 1B shows a schematic view of a green
ceramic laminate **100**, in this particular case and for the sole purpose of describing this
10 invention, made from 5 different metallized green sheets.

The present invention discloses that the addition of properly tailored non-
densifying structures, such as continuous thin metal structures, to the green ceramic
laminate kerf area improves the dimensional control of the ceramic product during the hot
pressing sintering process, and also allow for external pressure reduction. In addition to
15 shape, the location and thickness of these non-densifying structures must also be selected
properly to match the ceramic product **35** design features and the metallized green sheet
10 and laminate **100** characteristics and provide the desired inventive functionality.

In one embodiment, and referring to Figure 2A, the invention provides a method
to control global post sinter dimensions of a multi-up laminate during hot pressing
20 sintering by placing a continuous non-densifying structure **40** on a green sheet **10** in the
kerf area **30** between the individual products **35** prior to sintering and then separating the
continuous non-densifying structure **40** from the products **35** using post sinter wet sizing.

5 Referring to Figure 2B, one or more continuous non-densifying structures, for example **40** and **41**, are placed on one or more multi-up ceramic greensheets **10**, **12** in the kerf area **30** between the individual products **35**. The multi-up ceramic greensheets are stacked and laminated to form a multi-up green ceramic laminate **100** which is then green sized to separate external kerf area **20**, and then sintered wherein the continuous non-

10 densifying structures **40** and **41** will control the dimensions of the multilayer ceramic substrate. After sintering, the substrate will be diced into the individual products **35** separating the non-densifying structures **40** and **41** in the local kerf area **30** from each individual multilayer ceramic product **35**.

15 The continuous non-densifying structure **40** can accommodate discontinuities or small gaps in the shape as long as such gaps do not exceed 1 to 1.5 millimeters in size. These gaps are sometimes needed to provide a path for postsinter dicing processing and are allowed as long as the gap width is smaller than the length of the non-densifying structure **40** around the given gap.

20 In addition, for particular substrate designs containing local non-metallized regions within the metallized design area, individual discrete tailored shapes can be placed in available non-metallized regions as needed to control local distortion. These individual discrete tailored shapes would typically be made of the same material as the continuous non-densifying structure. Typical dimensions, as an example, include a

5 thickness ranging from 0.0003 inch to 0.001 inch, width in the range from 0.002 inch to 0.008 inch and a length determined by the area of the local non-metallized region.

10 In another embodiment, and referring to Figure 3A, the invention provides a method to control post sinter dimensions of individual products 35 in a multi-up laminate 100 during hot pressing sintering by placing a continuous non-densifying structure 41 in the kerf area 30 between the individual product ups prior to sintering and then separating the continuous non-densifying structure 41 from the product 35 using post sinter wet sizing. As shown in Figure 3B, one or more continuous non-densifying structures 41 are placed on one or more multi-up ceramic greensheets 10, 12 in the kerf area 30 between the individual products 35 with properly tailored shapes 51 to counterbalance local densification rate variability within the sintering laminate 100 created by the use of external pressure.

20 The multi-up ceramic greensheets are stacked and laminated to form a multi-up green ceramic laminate 100 which is then green sized to remove external kerf area 20 and then sintered wherein the continuous non-densifying structures 40 and 41 in conjunction with local non-densifying structures 51 will control the dimensions of the individual products 35 in the multilayer ceramic substrate. After sintering, the substrate will be diced into the individual product samples separating the non-densifying structures 40, 41, and 51 from each individual multilayer ceramic substrate product 35.

5 In another embodiment, and referring to Figure 4A, the invention provides a method to reduce the external sintering pressure required to maintain an acceptable dimensional control in MLC substrates manufactured as a multi-up laminate **100** by placing one or more continuous non-densifying structures **41** in the kerf area **30** of the green sheet **10** under sintering and then separating them from the product using post
10 sinter wet sizing process. In a typical hot press sintering process, only the top and bottom surfaces of the green laminate **100** are prevented from shrinking in the planar or x-y dimensions by friction forces with the hot press plates or sintering fixtures. The addition of non-densifying structures **41** inside the green laminate **100** provide additional planar
15 areas with frictional forces which reduce or prevent ceramic shrinkage also in x-y dimensions.

 Referring to Figure 4B, one or more continuous non-densifying structures, **40**, **41**, **42**, and **43**, are placed on one or more multi-up ceramic greensheets **10**, **12**, **13** and **14** in the kerf area **30** between the individual products **35**. In this case, the location and shape of the continuous non-densifying structure is selected and designed to reduce the vertical
20 distance between non-shrinking surfaces inside green laminate **100**, thus modifying the characteristics of the viscous deformation process step during the laminate densification. The multi-up ceramic greensheets are stacked and laminated to form a multi-up green ceramic laminate **100** which is then sintered wherein the continuous non-densifying

5 structures will control the dimensions of the individual products in the multilayer ceramic substrate. After sintering, the sintered laminate 100 will be sized into the individual products 35 separating the non-densifying structures from each individual multilayer ceramic substrate product 35.

10 In another embodiment of the invention, and referring to Figure 5A, a first continuous non-densifying structure 41 is used to control the distortion of a multi-up green ceramic laminate 100 during sintering while a second continuous non-densifying structure 60 is used to control the distortion of the individual products 35 during lamination. The first continuous non-densifying structure 41 is placed on one or more multi-up ceramic greensheets 10 in the area adjacent to the product area, kerf area 30, of
15 the individual ups.

The second continuous non-densifying structure 60 is placed on one or more multi-up ceramic greensheets 10 in the peripheral, external kerf area 20. As shown in Figure 5B the multi-up ceramic greensheets are stacked and laminated to form a multi-up green ceramic laminate 100 which is first green sized to produce a multi-up green
20 laminate and then sintered in a hot press. The second continuous non-densifying structure 60 is separated from the green laminate 100 during green sizing step, prior to sintering.

The first and second non-densifying structures will control the distortion of the

5 multi-up ceramic laminate during the lamination step by tailoring the green laminate
initial density distribution, then the first continuous non-densifying structure 41 will
control the distortion of the multi-up laminate during the hot pressing sintering step. Post
sintering, the multi-up substrate is diced to form individual product substrates and the
first continuous non-densifying structure is separated from the individual ceramic
10 substrates.

The continuous non-densifying structure can be made from, for example, copper,
molybdenum, tungsten, nickel, nickel alloys, stainless steel, dense alumina and zirconia.
The continuous non-densifying structure need not be a metal. Metal-ceramic composites,
polymers, or ceramic materials which are already densified may also be used. In general
15 metals and polymers have advantages over ceramics as materials for the continuous non-
densifying structure since metals and polymers can deform without breaking under load.

The dimensions of the continuous non-densifying structure is tailored to the
particular design of the product greensheets. It would be obvious to one skilled in the art
to adjust the dimensions of the continuous non-densifying structures for a particular
20 design. Typical dimensions, as an example, include a thickness ranging from 0.0003 inch
to 0.001 inch, and width greater than 0.5 millimeters.

5 While the present invention has been described with regard to a multi-up laminate it is not limited to a multi-up laminate. The present invention is also applicable to a single product laminate or one-up laminate, such as a multi-chip module (MCM).

10 It will be apparent to those skilled in the art having regard to this disclosure that other modifications of this invention beyond those embodiments specifically described here may be made without departing from the spirit of the invention. Accordingly, such modifications are considered within the scope of the invention as limited solely by the appended claims.